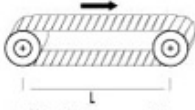
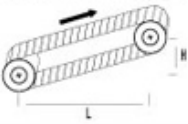


PASLANMAZ BANT SEÇİMİ/CHOICE OF STAINLESS STEEL CHAIN
**Yatay Konveyör
Horizontal conveyor**

**Eğimli Konveyör
Inclined conveyor**

**Doğrusal bant kullanılan konveyörlerde F_t 'nin bulunması
Conveyors with straight running chains**

$$F_t = (2W_c + W_m) \times L \times f_1 \times f_p \times 9,81$$

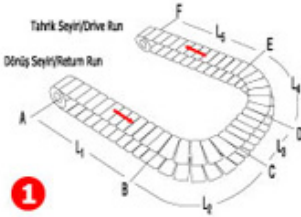
$$F_t = [(2W_c + W_m) \times L \times f_1 \times f_p + L_s \times W_m \times f_2 \times S] \times 9,81$$

$$F_t = [(2W_c + W_m) \times L \times f_1 \times f_p + (W_c + W_m) \times H] \times 9,81$$

$$F_t = [(2W_c + W_m) \times L \times f_1 \times f_p + (W_c + W_m) \times H] \times 9,81$$

Eşitliklerin sonucunda/As a result of equations

$$F_t = [(2W_c + W_m) \times L \times f_1 \times f_p + (W_c + W_m) \times H + L_s \times W_m \times f_2 \times S] \times 9,81$$

**Dönüşlü bant kullanılan konveyörlerde F_t 'nin bulunması
Conveyors with sidflexing chains 1**


Tahrik bölümündeki bant kuvvetlerinin toplamı sonuçundaki eşitlik toplam yüklemeyi verecektir.
In this case the calculation of the chain tension at headshaft is carried out as the sum of successive loads

$$L_2 = K(\alpha_2) \times R_2$$

$$L_4 = K(\alpha_4) \times R_4$$

Dönüş Seyiri/Return Run 2

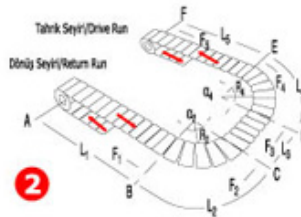
$$FE \quad F_5 = W_c \times L_5 \times f_1$$

$$FD \quad F_4 = [F_5 + W_c \times L_4 \times f_1] \times T(\alpha_4)$$

$$FC \quad F_3 = F_4 + W_c \times L_3 \times f_1$$

$$FB \quad F_2 = [F_3 + W_c \times L_2 \times f_1] \times T(\alpha_2)$$

$$FA \quad F_0 = F_1 + f_p \times 9,81$$



$$F_0 = \{[(L_5 + L_4) \times W_c \times f_1 \times T(\alpha_4) + (L_3 + L_2) \times W_c \times f_1] \times T(\alpha_4) + L_1 \times W_c \times f_1\} \times f_p \times 9,81$$

Tahrik Seyiri/Drive Run 3

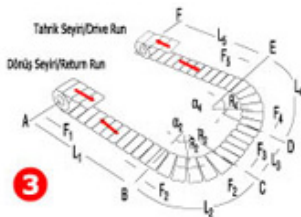
$$AB \quad F_1 = F_0 + (W_c + W_m) \times L_1 \times f_1 + f_p \times 9,81$$

$$AC \quad F_2 = \{F_1 + [(W_c + W_m) \times L_2 \times f_1 + f_p \times 9,81] \times T(\alpha_2)\}$$

$$AD \quad F_3 = F_2 + (W_c + W_m) \times L_3 \times f_1 + f_p \times 9,81$$

$$AE \quad F_4 = \{F_3 + [(W_c + W_m) \times L_4 \times f_1 + f_p \times 9,81] \times T(\alpha_4)\}$$

$$AF \quad F_5 = F_4 + (W_c + W_m) \times L_5 \times f_1 + f_p \times 9,81$$



$$AB \quad F_1 = F_0 + [(W_c + W_m) \times L_1 \times f_1 \times f_p + L_{1S} \times W_m \times f_2 \times S] \times 9,81$$

$$AC \quad F_2 = \{F_1 + [(W_c + W_m) \times L_2 \times f_1 \times f_p + L_{2S} \times W_m \times f_2 \times S] \times 9,81\} \times T(\alpha_2)$$

$$AD \quad F_3 = F_2 + [(W_c + W_m) \times L_3 \times f_1 \times f_p + L_{3S} \times W_m \times f_2 \times S] \times 9,81$$

$$AE \quad F_4 = \{F_3 + [(W_c + W_m) \times L_4 \times f_1 \times f_p + L_{4S} \times W_m \times f_2 \times S] \times 9,81\} \times T(\alpha_4)$$

$$AF \quad F_5 = F_4 + [(W_c + W_m) \times L_5 \times f_1 \times f_p + L_{5S} \times W_m \times f_2 \times S] \times 9,81$$